Revisiting Mg–Mg$_2$Ni System from Electronic Perspective

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Abstract: Both Mg and Mg$_2$Ni are promising electrode materials in conversion-type secondary batteries. Earlier studies have shown their single-phase prospects in electro-devices, while in this work, we have quantitatively reported the electronic properties of their dual-phase materials, that is, Mg–Mg$_2$Ni alloys, and analyzed the underlying reasons behind the property changes of materials. The hypoeutectic Mg–Mg$_2$Ni alloys are found to be evidently more conductive than the hypereutectic Mg–Mg$_2$Ni system. The density functional theory (DFT) calculations give the intrinsic origin of electronic structures of both Mg$_2$Ni and Mg. The morphology of quasi-nanoscale eutectics is another factor that can affect the electronic properties of the investigated alloy system; that is, the electrical property change of the investigated alloys system is due to a combination of the intrinsic property difference between the two constituting phases and the change of eutectic microstructures that affect electron scattering. In addition, regarding the Mg–Mg$_2$Ni alloy design for device applications, the electronic property and mechanical aspect should be well balanced.

Keywords: magnesium; electronic properties; electronic structures; DFT

1. Introduction

In the context of limited fossil-fuel reserves and their induced environmental pollution problems, green or renewable energy research has been a focus point all over the world. Among this research, one of the main trends is to use less traditional fuels and instead widen the usage of electricity, which can be generated from several renewable energy resources such as solar, wind, bio-mass, and so forth. Therefore, electrical energy storage is becoming an ever more important research topic. This issue is becoming more emphasized as the current utilization of electricity is moving from small-sized consumer electronics to large-scale electric vehicles, the smart grid and other industrial systems [1–6]. The technology of Li-ion or Na-ion batteries is a promising solution to tackle the energy storage problems, although the technology is still facing many challenges in meeting technical requirements and in cost-efficiency [7–13]. Differently from many traditional studies on electrode materials such as the intercalation type or the alloying type, Y. Oumellal et al. reported a new concept to use metal hydrides as conversion electrodes with high capacities for Li-ion battery applications [14,15]. Until now, some single-phase metal hydrides such as MgH$_2$ and Mg$_2$NiH$_4$ have been experimentally considered.
in related studies and have shown good electrochemical properties for battery conversion anode applications. Their conversion mechanism can be represented by the following reactions, respectively:

\[
\text{Mg} + 2\text{LiH} = \text{MgH}_2 + 2\text{Li}^+ + 2e^- \quad (1)
\]

\[
\text{Mg}_2\text{Ni} + 4\text{LiH} = 2\text{Mg}\text{NiH}_4 + 4\text{Li}^+ + 4e^- \quad (2)
\]

Because the electronic conductivity of LiH phase is poor, the Mg- or Mg\(_2\)Ni-phase would play an important role as an electrode conductor in their respective battery systems. This inspires one idea/question, that is, what will their electronic properties be if we combine the Mg- and Mg\(_2\)Ni-phase in the form of alloy? In order to find the answer, in this work we have fabricated several Mg–Mg\(_2\)Ni alloys with different compositions and aimed to unveil the relationship between the electronic properties and structures of the alloy system by means of experiments and density functional theory (DFT) calculations. This work is proposed to supply first-hand data on basic electronic properties of the Mg–Mg\(_2\)Ni alloy system and help to guide the choice of proper Mg–Mg\(_2\)Ni dual-phase material for secondary battery or other device applications.

2. Materials and Methods

The examined alloys were prepared in a 5 kW electric furnace using 99.85% commercial purity bulk Mg and Ni–20 wt % Mg master alloy. The RJ-2 flux containing mainly MgCl\(_2\) and KCl were used for melt protection and refining. Four compositions of Mg–Ni alloys (Mg–8.8Ni, Mg–14Ni, Mg–25.6Ni, and Mg–31Ni; all in wt % and marked as alloys A, B, C and D, respectively) together with pure Mg were designed and obtained in this work and were measured by means of a QSN750 spectrometer (OBLF company, Dortmund, Germany). After melting, the melts were respectively cast into a cylindrical steel mold preheated to 200 °C with size of \(\phi 25 \text{ mm} \times 60 \text{ mm}\). For microstructural analysis and comparison, all samples were taken from the middle position along the radius direction of the ingots. A Hitachi-430 field emission gun scanning electron microscope (FEG-SEM) affiliated with energy-dispersive X-ray spectroscopy (EDX) was employed to characterize the microstructures of the alloys. The electronic conductivity measurements were taken using a RS.03-DX200H electrical resistivity meter (Honghu company, Xi’an, China) according to the ASTM B193 standard. The hardness test bars were machined to the cube-type specimens (30 mm \(\times\) 20 mm \(\times\) 20 mm) and then tested on a HBS-3000 digital Brinell hardness tester according to the ASTM E10-14 standard.

The electronic structure calculations were performed using DFT [16,17] spin-polarized calculations with the projector augmented-wave (PAW) method [18], as implemented in the Vienna Ab initio simulation package [19,20]. The exchange-correlation interaction was considered in a generalized gradient approximation using the Perdew–Burke–Ernzerhof (PBE) scheme [21]. A K-points mesh of \(21 \times 21 \times 7\) was used in calculations and a plane-wave basis set with an energy cutoff of 500 eV was employed to describe the electronic wave function. The geometry optimization was done by minimizing the forces on atoms with a conjugate gradient algorithm and simultaneously minimizing stresses on unit cells without any symmetry constraint. An electronic convergence criterion of 0.00001 eV and ionic relaxation convergence criterion of 0.002 eV/Å were employed in the work. During the calculations, the spin polarization was considered. An electron localization function analysis was performed on the basis of the quantum solid state theory.

3. Results and Discussion

The microstructure of the fabricated Mg–8.8Ni alloy is shown in Figure 1a, from which it can be seen that the alloy consists of the primary Mg-phase and the eutectic region. The size of the precipitated primary Mg-phase during solidification is large and the dendrites constitute the majority of the volume fractions in the alloy. Figure 1b shows the magnified microstructure of the eutectic region. It was found that a lamellar eutectic structure is formed in the Mg–Mg\(_2\)Ni system, in which the white and black plate-like phases are eutectic Mg\(_2\)Ni and eutectic Mg-phase, respectively. It is interesting that the
spacing between alternated congeneric phases in the lamellar eutectic is of the quasi-nanoscale and that there occurs some growth orientation inside the eutectic colony.

![Figure 1](image1.png)

**Figure 1.** (a) Microstructure of Mg–8.8Ni alloy (designated as alloy A in this study), and (b) the magnified scanning electron microscopy image of the eutectic region.

The microstructure of the Mg–14Ni alloy with an increase in the content of Ni in the alloy is shown in Figure 2a. It can be seen that the microstructure is still hypoeutectic with the primary Mg-phase and eutectic region, while the difference is that the size of the primary Mg-phase becomes smaller compared with that in alloy A and the volume fraction of the eutectic region in alloy B becomes larger. Figure 2b represents the microstructure of the Mg–Mg$_2$Ni eutectic region, from which it can be found that the growth orientation of the eutectic phases is not evident in this alloy. Compared with the case in alloy A, the eutectic phase spacing is still of the quasi-nanoscale, but the eutectic structure is characterized by being undirectional.

![Figure 2](image2.png)

**Figure 2.** (a) Microstructure of Mg–14Ni alloy (designated as alloy B), and (b) the magnified scanning electron microscopy image of the eutectic region.

The microstructure of the Mg–25.6Ni alloy is shown in Figure 3. Evidently, the alloy becomes hypereutectic in this composition. The primary phase is no longer the Mg-phase and instead is primary Mg$_2$Ni characterized by a sharp rod-like morphology. The EDX analysis confirms the phase has an average length of around 40 μm. Besides the primary Mg$_2$Ni, the eutectic region also constitutes the whole microstructure of the alloy. Similarly to alloy A, the eutectic structure in alloy C is also lamellar with eutectic Mg$_2$Ni and eutectic Mg-phases arranged alternatively. There exists local growth orientation inside the eutectic colony in alloy C.
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Figure 3. (a) Microstructure of Mg–25.6Ni alloy (designated as alloy C), and (b) the morphology and energy-dispersive X-ray spectroscopy result of the primary Mg$_2$Ni.

Figure 4a illustrates the microstructure of the Mg–31Ni alloy, for which the content of Ni is further increased. Compared with the case in alloy C, it can be seen that both the amount and the size of the primary Mg$_2$Ni phases become larger in alloy D. Figure 4b shows the magnified structure of the eutectic region. It is found that the (Mg + Mg$_2$Ni) eutectics are characterized by a kind of “tendon-like” intersection with quasi-nanoscale lamellar spacing. The growth orientation is evident inside the local eutectic colony.

Figure 4. (a) Microstructure of Mg–31Ni alloy (designated as alloy D), and (b) the morphology of the eutectic region.

After comparing the microstructures of above alloys, we measured their electrical properties, and Figure 5 shows the results of electronic conductivity. It can evidently be seen that all the alloys are less conductive than pure Mg. With the increase of the Ni content in the alloy, the material system shows a declining trend in the electronic conductivity. Particularly, when the amount of primary Mg$_2$Ni is the greatest in alloy D, the electronic conductivity is only 15 IACS% (International Annealed Copper Standard) with a decrease of 60% compared with pure Mg. For battery electrode applications, one of the most important properties is electronic conductivity. Thus, from this perspective, the future Mg–Mg$_2$Ni alloy electrode should not contain a great deal of primary Mg$_2$Ni but should instead try to maintain a hypoeutectic composition.
From quantum theory, the electronic structure is the origin of electrical properties. We have calculated the electronic structures of both Mg and Mg$_2$Ni using DFT. The atomic and electronic structure of Mg$_2$Ni is shown in Figure 6. The calculated equilibrium crystal structure ($P6_222$ space group) of Mg$_2$Ni is illustrated in Figure 6a. The unit cell consists of 18 atoms with Mg atoms having 4 occupation sites and Ni atoms having 2 sites, which are labelled in the figure. Figure 6b shows the calculated electron localization function (ELF) isosurface with the nature of metallic bonding but illustrates some electron localization in red, which is negatively related to the electron transfer in materials. The total and partial density of states (DOS) is seen in Figure 6c. The total DOS is mainly contributed by the s states of Mg atoms and the d state of Ni2 atoms. There occurs orbital hybridization between the d orbital of Ni2 atoms and the p orbitals of Mg2 or Mg4 atoms, which contributes to the Mg–Ni chemical bonding. As seen from the DOS of Mg$_2$Ni, there are not many states available for occupation at the Fermi level. Figure 7a,b represents the unit cell and calculated ELF of pure Mg (hcp structure). With metallic bonding, the free electrons in Mg contribute greatly to its electrical conductivity. Figure 7c is the calculated total and partial DOS of pure Mg. The p state of Mg contributes the most to the total DOS at the Fermi level.
Figure 6. (a) The calculated equilibrium crystal structure, (b) electron localization function (isosurface level of 0.285), and (c) electronic density of states of Mg$_2$Ni (the Fermi level is set at zero).

Figure 7. (a) The unit cell, (b) the calculated electron localization function (isosurface level of 0.567), and (c) electronic density of states of pure Mg (the Fermi level is set at zero).
Besides the above analysis of the electronic structures’ nature, the microstructure scale of the alloys can also affect their electrical properties. Taking alloy B as an example, the disordered arrangement of the eutectics will scatter electrons more than the oriented eutectic structure in alloy A. Alloy D is another typical material to be discussed. When we analyze its low electronic conductivity, two main factors should be considered: the intrinsic property of the primary Mg$_2$Ni-phase and the morphology of eutectics. As is known from the above, the intrinsic Mg$_2$Ni-phase is less conductive than the Mg phase. In addition, the “tendon-like” intersection of eutectics that cause severe electron scattering in the alloy is also not beneficial for electronic conductivity.

From the above results, it seems that alloy A with a higher electronic conductivity than the other alloys is the best choice for the battery electrode. However, the electrode material should also have good mechanical properties. Thus, hardness testing of these Mg–Mg$_2$Ni alloys has also been carried out. Figure 8a shows the Brinell hardness comparison, from which it can be seen that the hardness of the alloy is enhanced with an increase in the Ni content; that is, the existence of primary Mg$_2$Ni improves the mechanical hardness of the alloy more so than for the primary Mg-phase. These experimentally measured results correspond qualitatively with the DFT calculations. Figure 8b gives the cohesive energies of pure Mg and Mg$_2$Ni, which can reflect the bonding strength of the matter. The calculations are based on the formula below:

\[
E_{\text{coh}} = \frac{[E(A_xB_y) - xE(A) - yE(B)]}{(x + y)}
\]  

(3)

where $E(A_xB_y)$ is the total energy of the matter $A_xB_y$, while $E(A)$ and $E(B)$ stand for the spin-polarized ground-state total energies of atoms A and B, respectively. Evidently, the value of Mg$_2$Ni is more negative (−2.869 eV). This makes Mg$_2$Ni act stronger when the alloy is under mechanical load. The properties of electronic conductivity and mechanical hardness should be well balanced when choosing the right composition in a Mg–Mg$_2$Ni alloy system for device electrode applications.

![Figure 8. (a) Brinell hardness of the investigated Mg–Mg$_2$Ni alloy system, and (b) the calculated cohesive energies of Mg and Mg$_2$Ni from density functional theory.](image)

4. Summary and Outlook

In this study, the microstructures and electrical properties of several hypoeutectic and hypereutectic Mg–Mg$_2$Ni alloys have been investigated, and the structure–property relationship has also been analyzed. In hypereutectic Mg–Mg$_2$Ni alloy, the primary Mg$_2$Ni-phase is characterized by a sharp rod-like morphology. As for the eutectic structure in the alloy, the quasi-nanoscale spacing between the eutectic Mg-phase and eutectic Mg$_2$Ni-phase has been found. DFT calculations revealed the superior electronic conductivity of Mg over Mg$_2$Ni, which makes the electrical property of the hypoeutectic Mg–Mg$_2$Ni alloy system better than that of the hypereutectic alloy system. Besides the property of good electrical conductivity that the battery material should have, the mechanical property has also been assessed and balanced among the studied alloys. It is proposed that this study creates a
new perspective to investigate the Mg–Mg$_2$Ni system and will encourage more research to focus on this alloy system for electro-device or other functional applications.

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**Author Contributions:** Zhao Qian conceived and designed the study; Zhao Qian, Weimin Guo, Guanzhong Jiang and Shaokun Xu performed the experiments and calculations; Zhao Qian, Rajeev Ahuja and Xiangfa Liu analyzed the data; Zhao Qian wrote the paper.

**Conflicts of Interest:** The authors declare no conflict of interest.

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