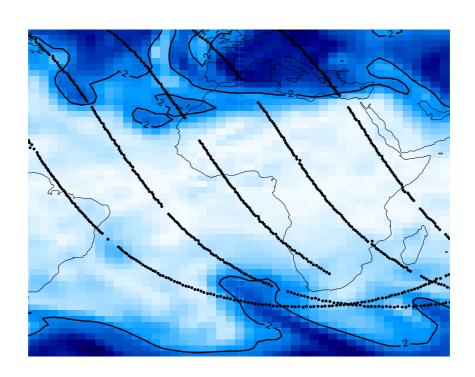
# Instrumental Requirements for a Submillimeter-Wave Limb Sounder

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#### **Overview**

- Motivation
- Retrieval method
- Error analysis: The linear mapping method
- The SOPRANO instrument
- Antenna
  - Antenna efficiency
  - Far wing knowledge
- Pointing
  - Pointing accuracy
  - Pointing stability
- Radiometric errors
  - Baseline ripples
  - Baseline discontinuities
  - Calibration errors
- Error summary for selected species
- Conclusions
- Ongoing work



### **Motivation**

- Which instrument parameters are crucial for the scientific goal?
- Minimize systematic errors
- Optimize performance



### Retrieval by optimal estimation

- Described in: Rodgers, C. D., Journal of Geophysical Research, 95, 5587-5595, 1990.
- Minimize:

$$\chi^{2}_{\text{OEM}} = [\vec{y} - F(\vec{x})] \mathbf{S}_{\vec{y}}^{-1} [\vec{y} - F(\vec{x})] + [\vec{x} - \vec{x}_{a}] \mathbf{S}_{\vec{x}_{a}}^{-1} [\vec{x} - \vec{x}_{a}]$$

 $\vec{x}$  : state vector

 $ec{x}_a$  : a priori

 $\mathbf{S}_{\vec{x}_a}$  : a priori covariance matrix  $\vec{y}$  : measurement

 $F(\vec{x})$  : forward model

 $\mathbf{S}_{\vec{v}}$  : meas. covariance matrix

 We use the Levenberg-Marquardt method to find the minimum



# Method of investigation

 Impact of instrument parameters on the retrieval investigated by linear mapping:

$$\mathbf{D} = \partial \hat{\mathbf{x}} / \partial \mathbf{y}$$

D: Contribution function matrix

x : Retrieved atmospheric profile

y: Measured spectrum

• Impact on retrieval then given as

$$\Delta \hat{\mathbf{x}} = \mathbf{D} \Delta \mathbf{y}$$

 Generate ensembles of 100 or 1000 cases and calculate RMS error.



# **The SOPRANO Instrument**

Band	f [GHz]	Species
A	497.5 – 504.75	O <sub>3</sub> , CIO, CH <sub>3</sub> CI, (BrO), N <sub>2</sub> O, H <sub>2</sub> O, (HNO <sub>3</sub> ), (COF <sub>2</sub> )
B1	624.6 – 626.5	<b>HCI</b> , $O_3$ , HOCI, (HNO <sub>3</sub> ), (BrO), (HO <sub>2</sub> )
B2	627.95 – 628.95	<b>HOCI</b> , $O_3$ , $HNO_3$ , $(COF_2)$
C1	635.6 – 637.4	CH <sub>3</sub> CI, O <sub>3</sub> , HNO <sub>3</sub> , HOCI, HO <sub>2</sub>
C2	648.0 – 652.0	<b>CIO</b> , <b>O</b> <sub>3</sub> , N <sub>2</sub> O, HNO <sub>3</sub> , (H <sub>2</sub> CO), (HOCI), (HO <sub>2</sub> ), (NO <sub>2</sub> ), (BrO)
D	730.8 – 732.25	T, O <sub>3</sub> , Scan, HNO <sub>3</sub> , (CH <sub>3</sub> Cl), (HO <sub>2</sub> )
E	851.5 – 852.5	<b>NO</b> , O <sub>3</sub> , N <sub>2</sub> O, (HNO <sub>3</sub> ), (NO <sub>2</sub> ), (H <sub>2</sub> O <sub>2</sub> )
F	952.0 — 955.0	<b>NO</b> , <b>T</b> , Scan, O <sub>3</sub> , N <sub>2</sub> O, (HO <sub>2</sub> ), (HNO <sub>3</sub> ), (CH <sub>3</sub> Cl), (NO <sub>2</sub> )
G1	685.5 – 687.2	<b>CIO</b> , O <sub>3</sub> , (HNO <sub>3</sub> ), (HOCI), (H <sub>2</sub> O <sub>2</sub> ), (COF <sub>2</sub> ), (NO <sub>2</sub> )
G2	688.5 – 692.0	<b>CO</b> , <b>CH</b> <sub>3</sub> <b>CI</b> , CIO, O <sub>3</sub> , HNO <sub>3</sub> , (HO <sub>2</sub> ), (HOCI), (HCN), (NO <sub>2</sub> ), (H <sub>2</sub> O)



#### **Antenna**

**Assumed full width** at -3 dB around a typical tangent point:  $\approx$  **2.7 km**. (SOPRANO antenna)

(Should be about 12% narrower for JEM/SMILES if one takes into account only platform altitude and antenna diameter.)

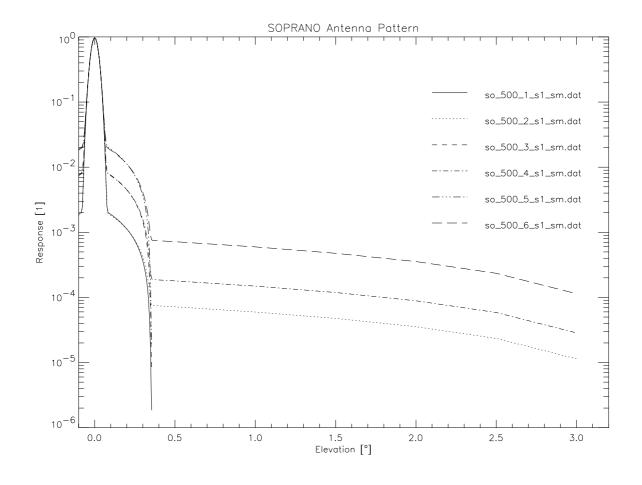
#### Investigation of:

- Perfectly known antenna pattern: How important is a good antenna efficiency (small near and far wing)?
- Imperfect antenna knowledge



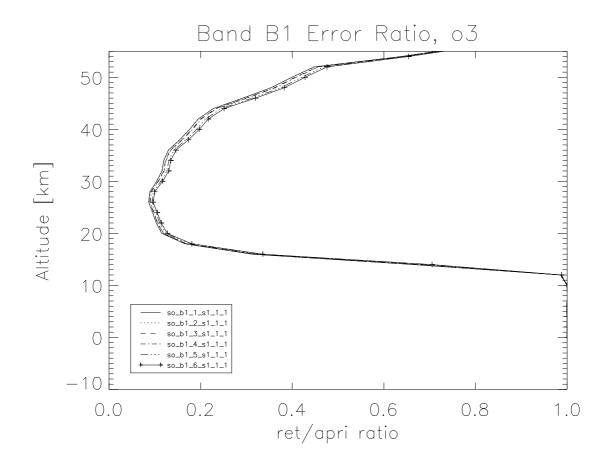
# Near and far wings

Case	Integration [%]		
	Near Wing	Far Wing	
1	1.0	0.0	
2	1.0	0.4	
3	4.0	0.0	
4	4.0	1.0	
5	10.0	0.0	
6	10.0	4.0	





### Near and far wings: O<sub>3</sub> near 625 GHz





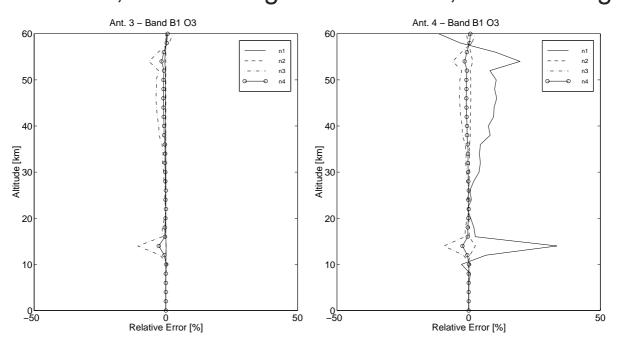
under the assumption that the antenna response is perfectly known throughout near and far wing.



# Imperfect antenna knowledge

4% near, 0% far wing

4% near, 1% far wing

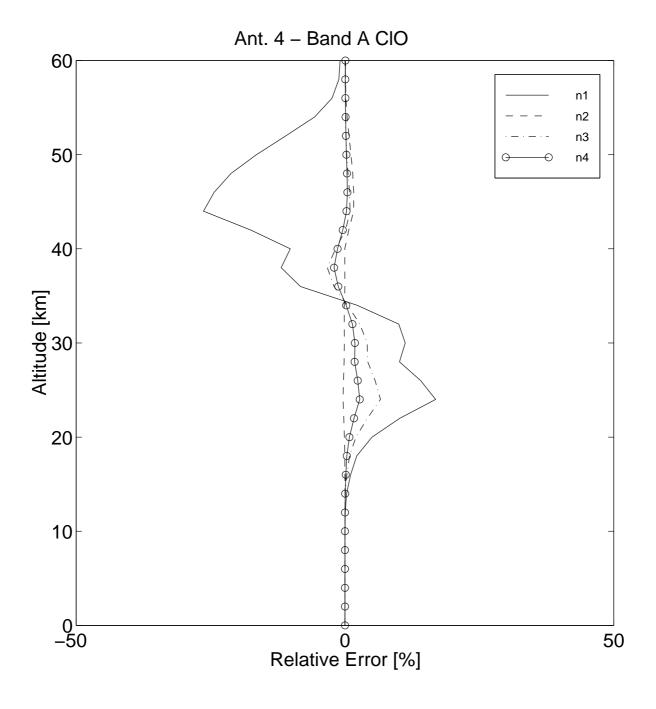


- n1: Antenna pattern measured with 20 dB non-linearity, 35 dB noise
- **n2**: Antenna pattern measured with 30 dB non-linearity, 45 dB noise
- **n3**:  $10\mu$ m antenna distortion
- n4: 0.25 times the effect of n3



# Imperfect knowledge: CIO near 500 GHz

• 4% near wing, 1% far wing





# Imperfect knowledge: Conclusions

- If there is a significant far wing it must be covered by the antenna measurement
- An antenna distortion of 10  $\mu$ m is not critical

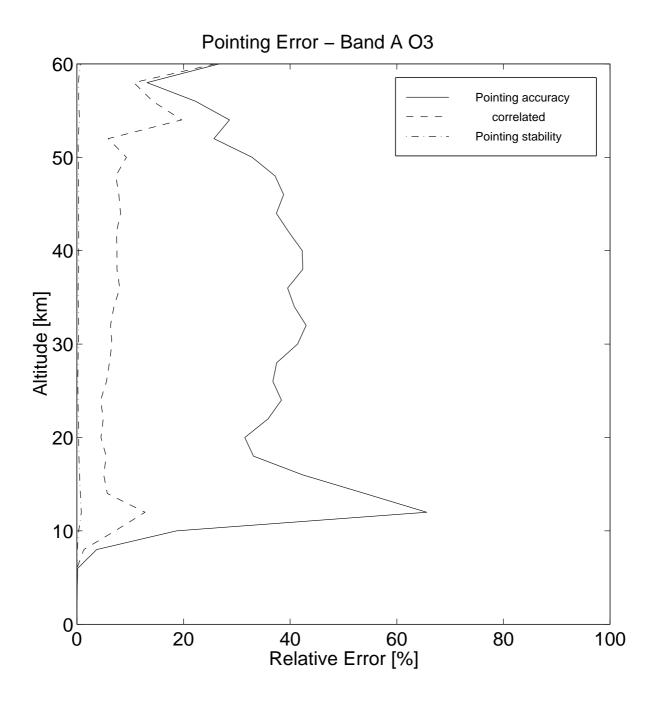


### **Pointing**

- Pointing accuracy: Two cases studied:
  - $-\pm 200\,\mathrm{m}$  random pointing offsets
  - Correlated random pointing with 200 m RMS (convolved first case with 6 km FWHM filter and scaled to 200 m RMS)
    Can be achieved technically by increased delay in antenna control loop
- Pointing stability (small scale pointing variations):
  - Simulated with different effective antenna patterns (± 200 m)
- Coregistration error: Scan offset of 200 m between different bands assumed
  - With and without scan offset fit

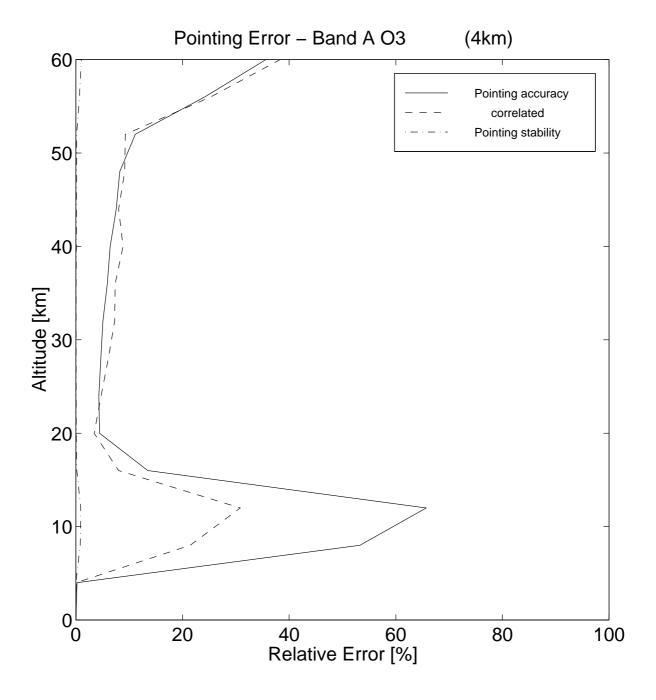


# Pointing: Ozone Band A (near 500 GHz)





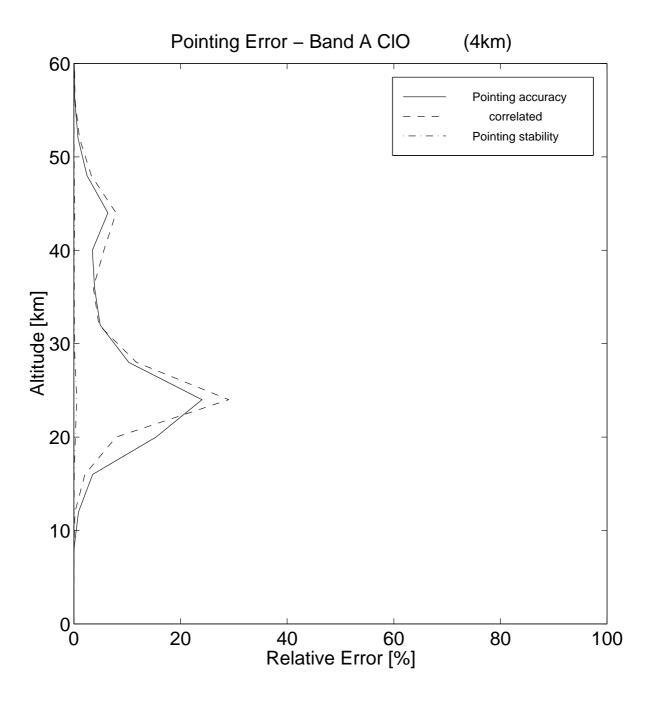
# Pointing: Ozone on 4 km retrieval grid



4 km retrieval grid reduces impact

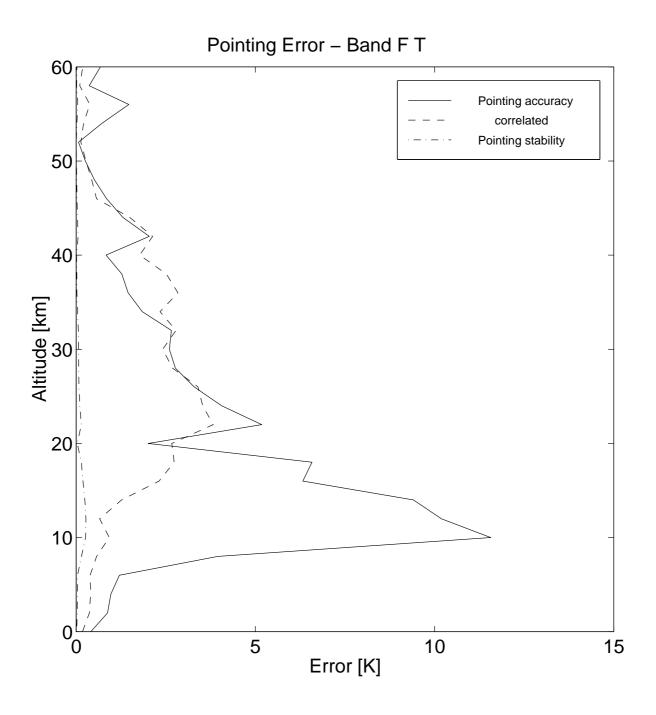


# Pointing: CIO Band A (near 500 GHz)



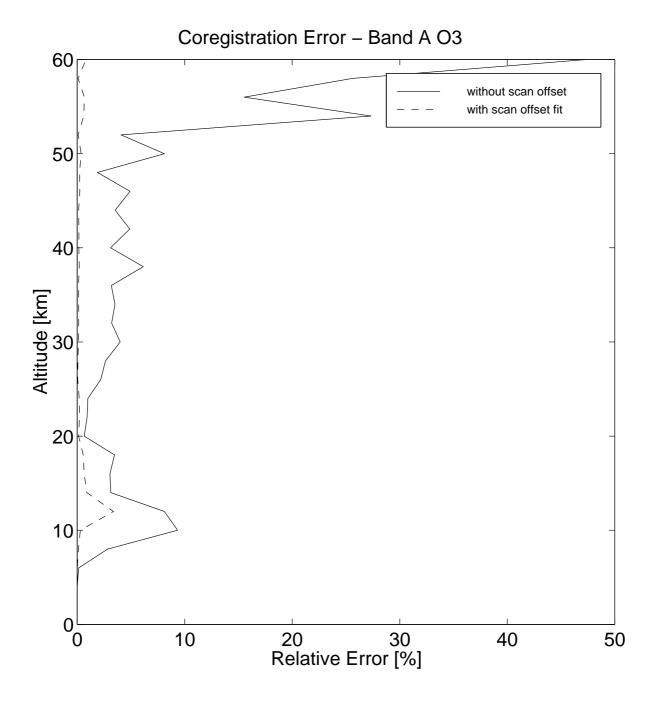


# Pointing: Temperature Band F (near 954 GHz)



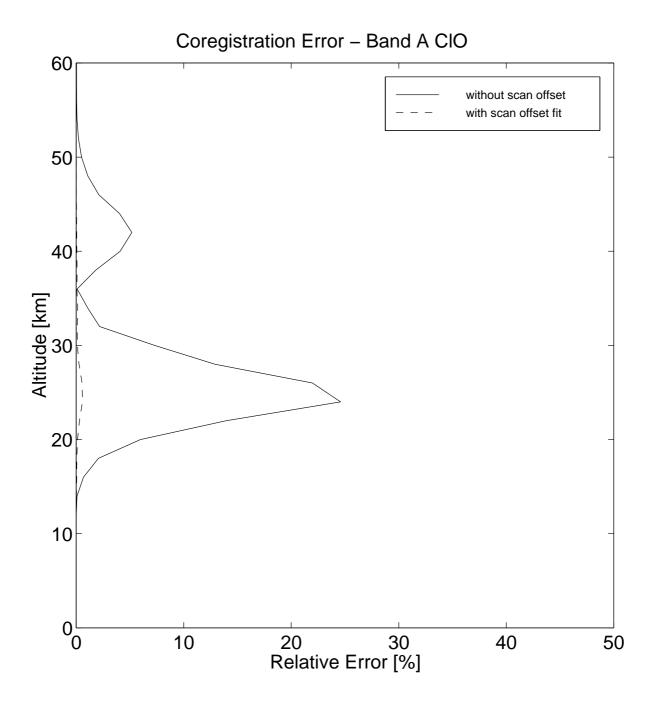


# Coregistration error: Ozone Band A (near 500 GHz)





# Coregistration error: CIO Band A





# **Pointing: Conclusions**

#### Pointing accuracy:

- ± 200 m has very critical impact on retrieval
- Impact can be reduced by: either
  - Correlated pointing error (corresponding to increased delay in antenna control loop)

or

- 4 km retrieval grid

but

 Doing both gives no additional improvement (actually 4 km grid retrievals are often even slightly better with uncorrelated pointing errors)



### **Pointing: Conclusions continued**

#### **Pointing stability:**

•  $\pm 200$  m not critical

#### **Coregistration error:**

- $\bullet$   $\pm$  200 m coregistration error has large impact
- ... but can be minimized with scan offset fit
- → Not critical



#### Radiometric errors

- Baseline ripples
- Baseline discontinuities
- Unwanted sideband
- Calibration errors
- Correlated noise



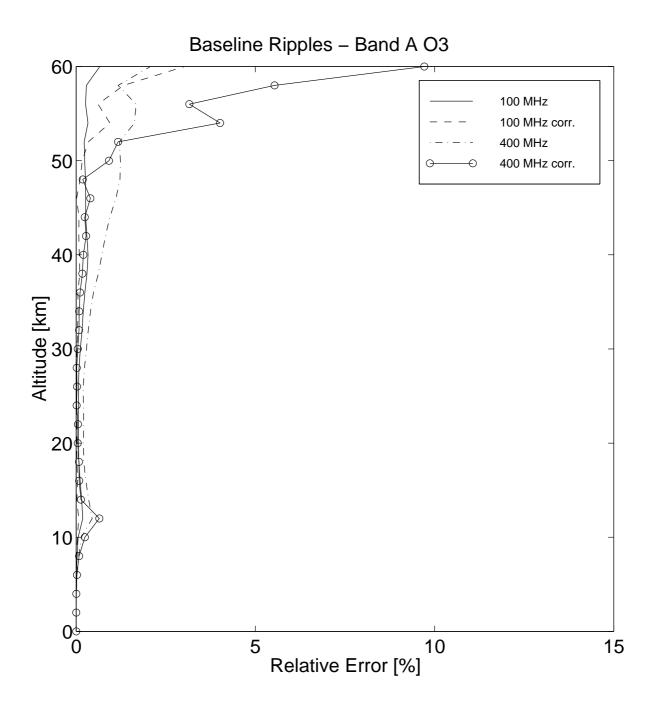
### **Baseline ripples**

#### **Assumptions:**

- Sinusoidal baseline structure
- 0.1 K amplitude
- 100 and 400 MHz periods
- Phase randomly distributed
- Two cases:
  - Phase constant during scan
  - Phase randomly distributed during scan

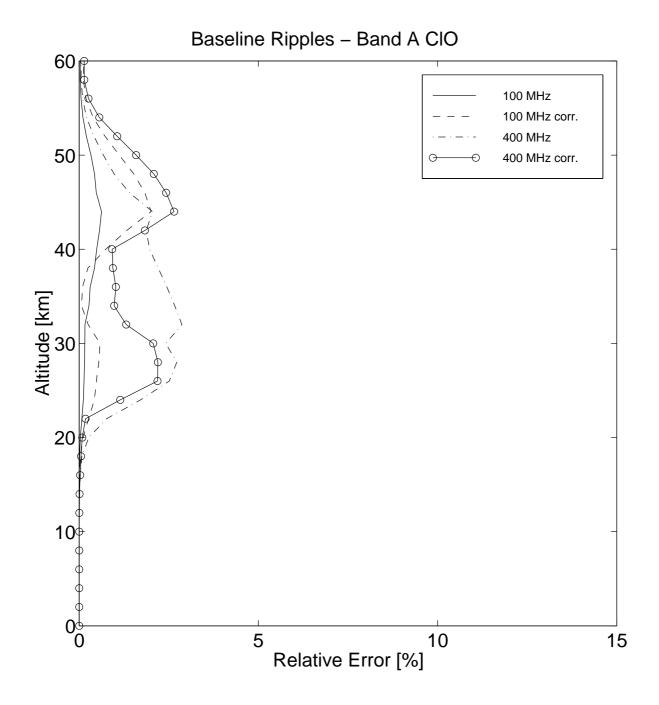


# Baseline ripples: Ozone Band A (near 500 GHz)





# **Baseline ripples: CIO Band A**





# **Baseline ripples: Conclusions**

- Impact of 400 MHz periods larger than 100 MHz periods
- Not critical
- However: 0.1 K seems optimistic



#### **Baseline discontinuities**

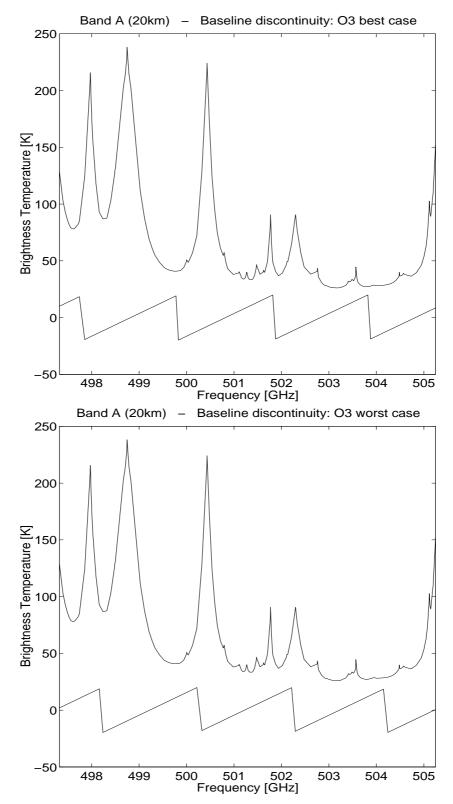
... may be caused by AOS modules

#### **Assumptions:**

- Simulated by sawtooth function from -0.2 K to +0.2 K every 2 GHz
- Phase shifted by 100 MHz → 20 cases

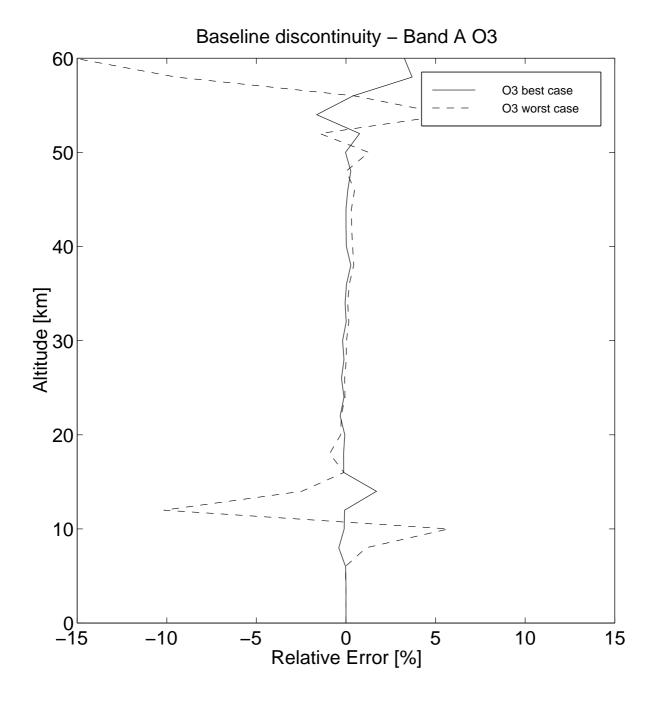


# Baseline discontinuity: O<sub>3</sub> Band A



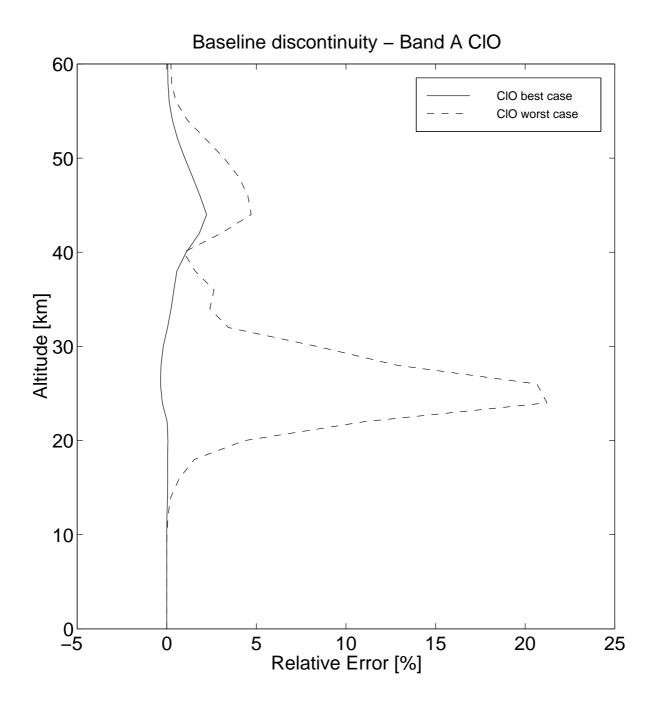


# Baseline discontinuity: O<sub>3</sub> Band A





# **Baseline discontinuity: CIO Band A**





### **Baseline discontinuity: Conclusions**

- Worst case for discontinuity near center of line of interest
- Impact stronger for weak lines
- Impact can be minimized by appropriate placement of AOS modules



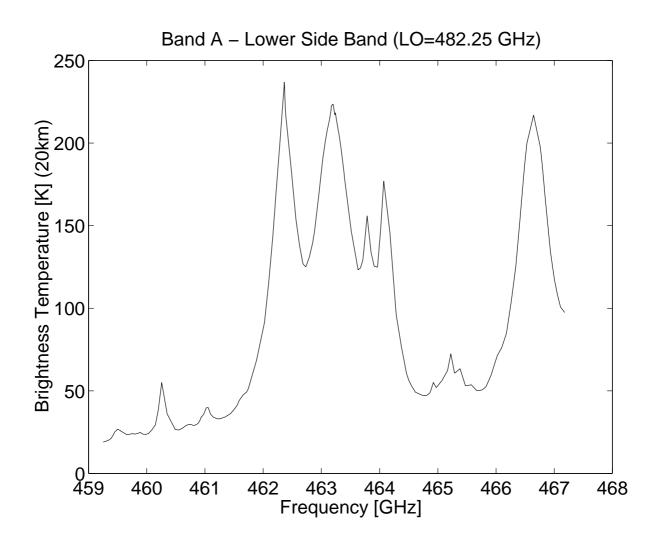
#### **Unwanted sideband**

- Nominal 20 dB suppression
- → 200 K line in sideband will appear with 2 K in measured spectrum!
- Impact depends on LO frequencies
- For SOPRANO study Dornier setup:

Band	LO frequency [GHz]
Α	482.25
B1	606.65
B2	606.65
F	933.50



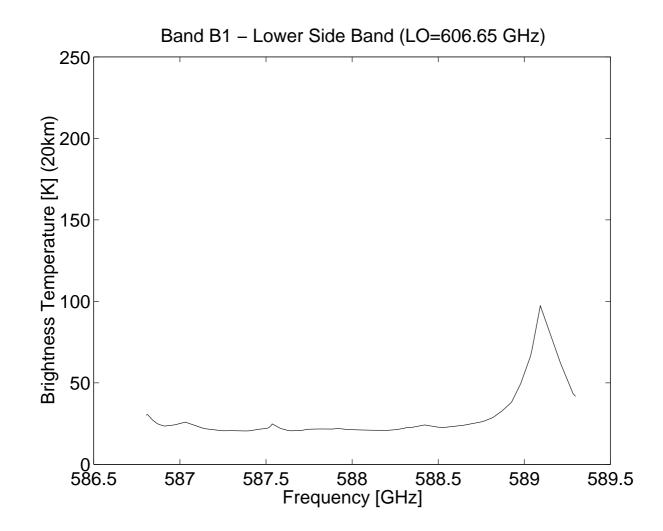
# Lower Sideband: Band A (near 500 GHz)



Many strong lines!



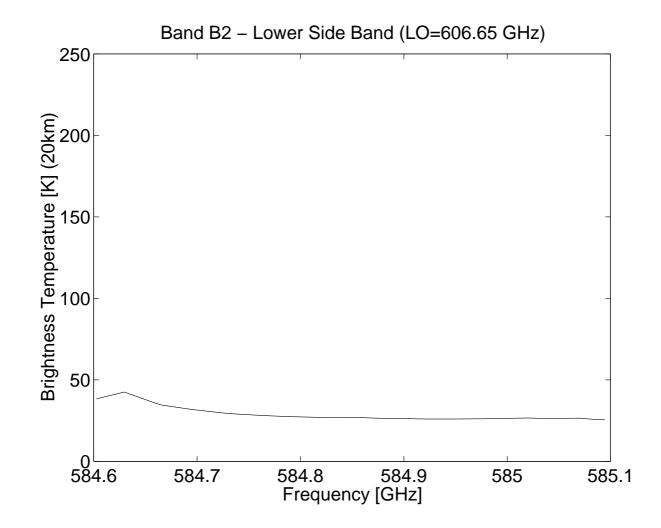
# Lower Sideband: Band B1 (near 625 GHz)



• Little structure

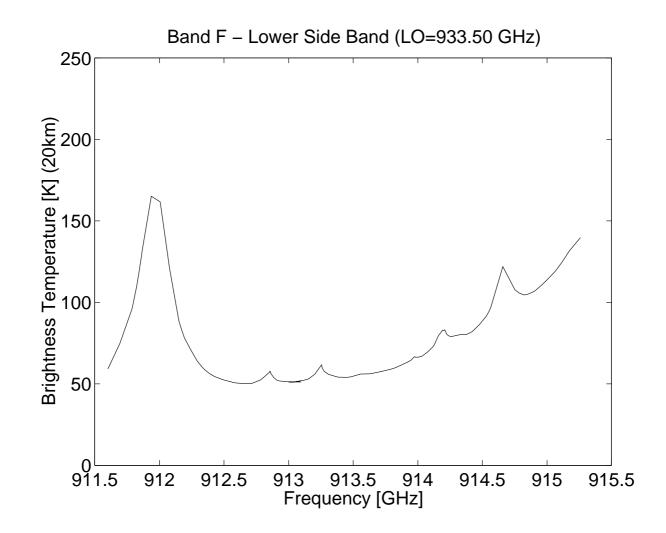


# Lower Sideband: Band B2 (near 628 GHz)





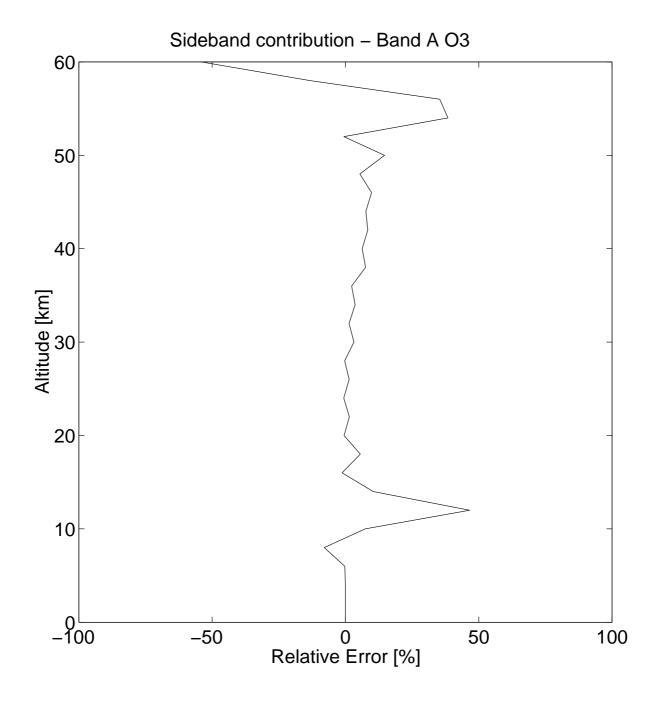
# Lower Sideband: Band F (near 954 GHz)



Moderate structure

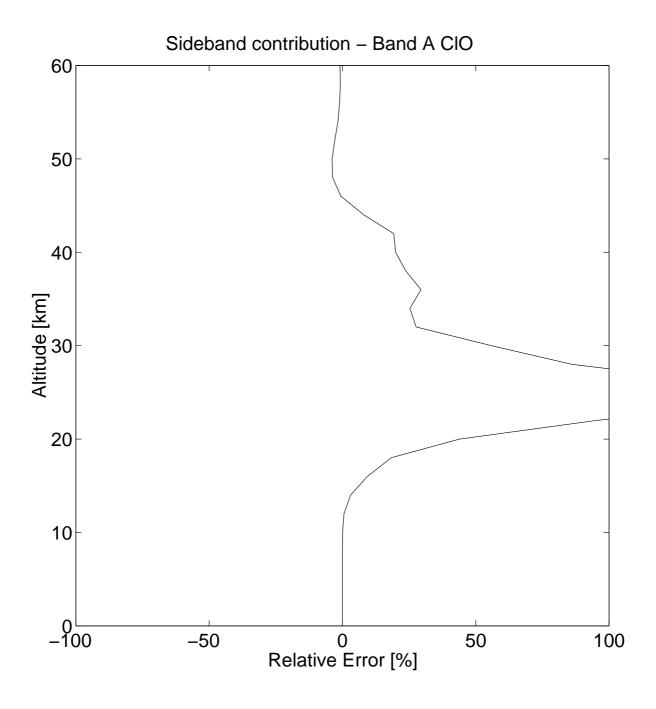


# Unwanted Sideband: Ozone Band A (near 500 GHz)





### **Unwanted Sideband: CIO Band A**





#### **Unwanted Sideband: Conclusions**

- Severe impact if uncorrected
- Dornier setup LO frequencies not optimal
  - Especially Band A should be optimized
- Impact can be corrected to first order if sideband ratio is known
- Present results can also be interpreted as error due to 20 dB knowledge of sideband ratio



#### **Calibration**

### Calibration process:

$$T_a = G(T_h - T_c) + T_c$$

with

$$G = (V_a - V_c)/(V_h - V_c)$$

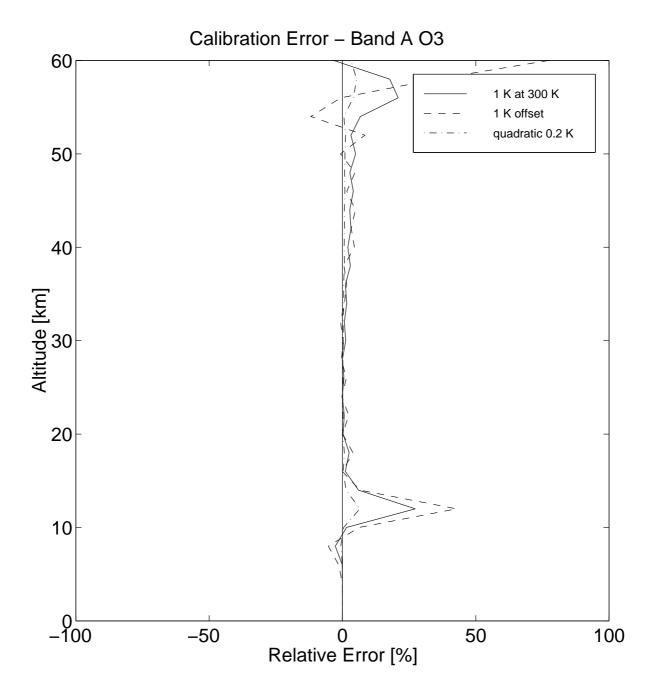
$$\longrightarrow \Delta T_a = \frac{T_a - T_c}{T_h - T_c} (\Delta T_h - \Delta T_c) + \Delta T_c$$

#### Three cases studied:

- 1 K error at 300 K
- 1 K offset
- Quadratic error of 0.2 K at 150 K

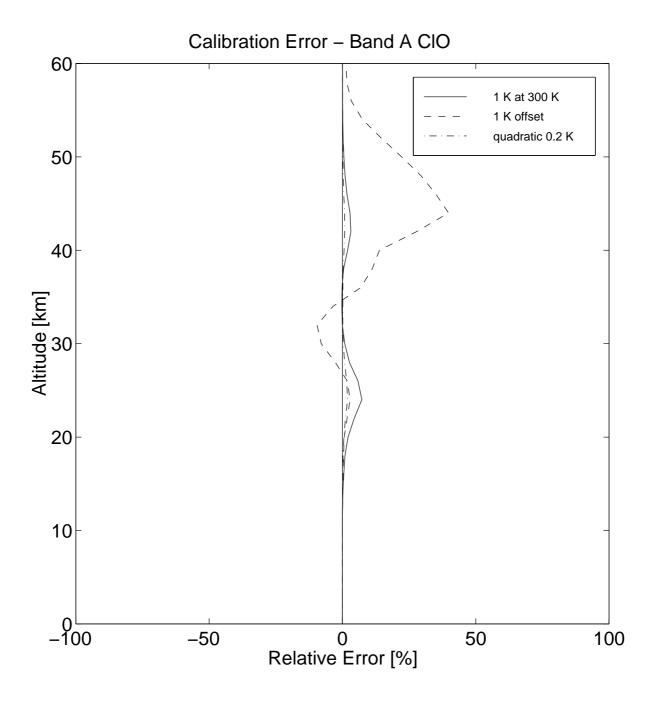


### Calibration error: Ozone Band A





### Calibration error: CIO Band A





### **Calibration error: Conclusions**

- 1 K offset introduces errors of 10% and larger
- Impact of 0.2 K quadratic error is small (because the quadratic error itself is assumed to be small)



#### **Correlated noise**

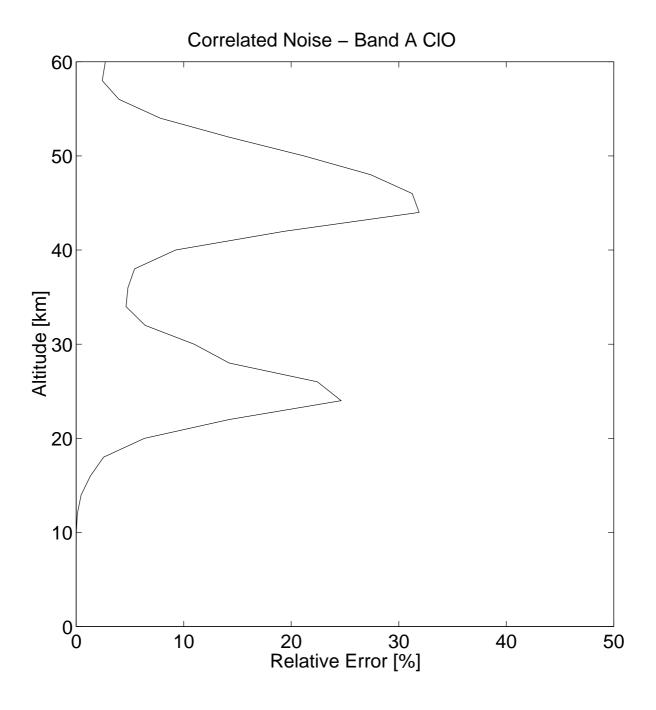
- Noise on calibration measurements will be correlated for each level during one scan
- Here an integration time of 2 sec. was assumed ( $10 \times$  atmospheric integration time)

#### Result:

- Errors same order of magnitude as measurement noise
- Statistical error: Decreases with averaging



### Correlated noise: CIO Band A





### **Temperature uncertainty**

Temperature weighting function:

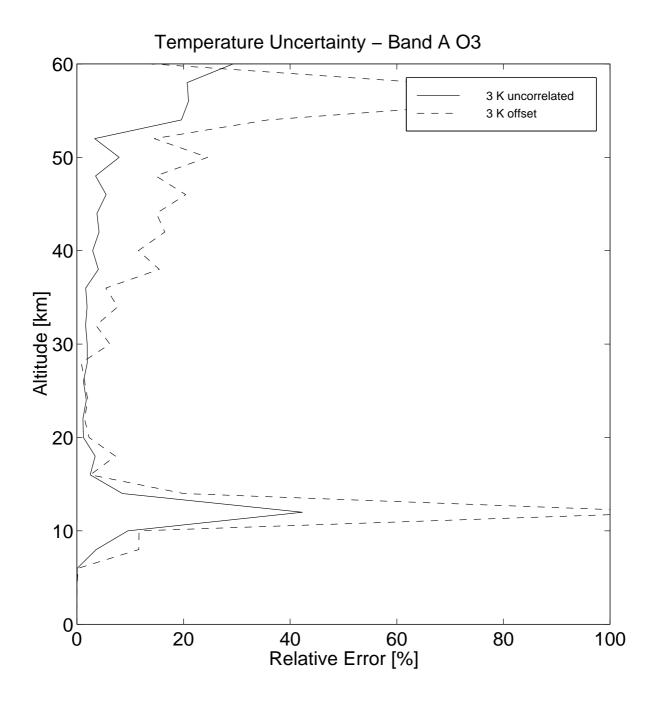
$$\mathbf{K}_b \equiv \frac{\partial F}{\partial b} \bigg|_{b=\bar{b}}$$

$$\mathbf{S}_S = \mathbf{D}\mathbf{K}_b \, \mathbf{S}_b \, (\mathbf{D}\mathbf{K}_b)^T$$

Two cases for  $S_b$  studied:

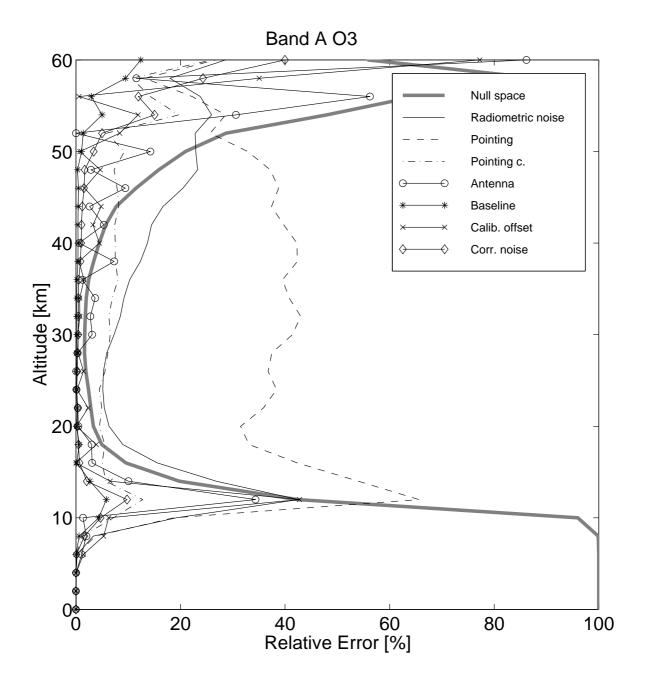
- 3 K uncorrelated
- 3 K offset

## Temperature uncertainty: Ozone Band A



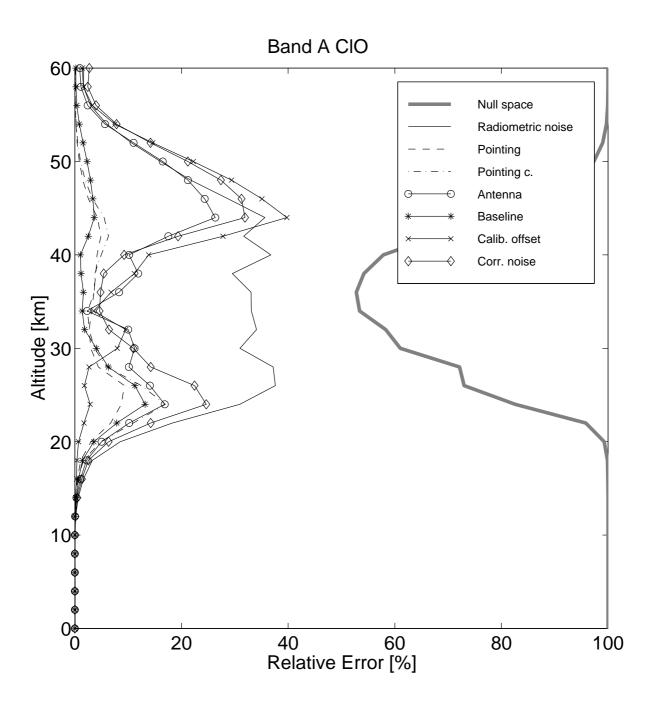


## Summary: Ozone Band A (near 500 GHz)



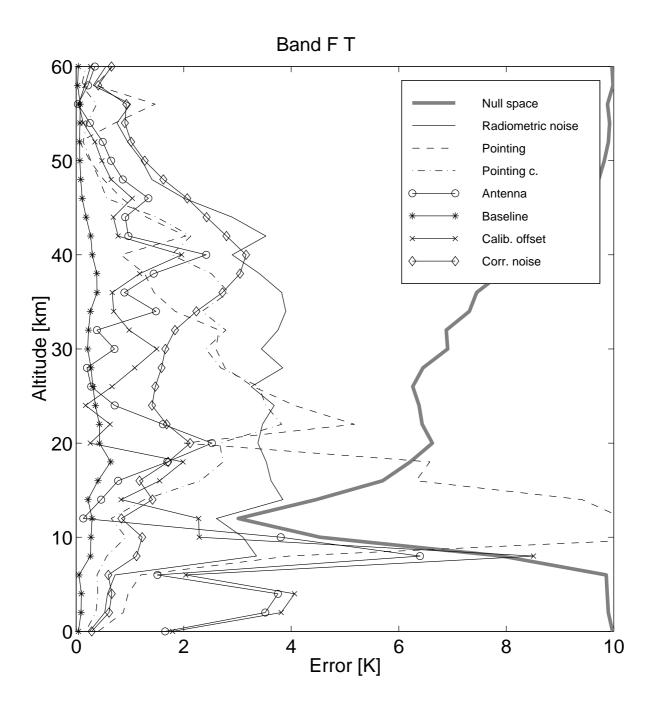


## Summary: CIO Band A (near 500 GHz)



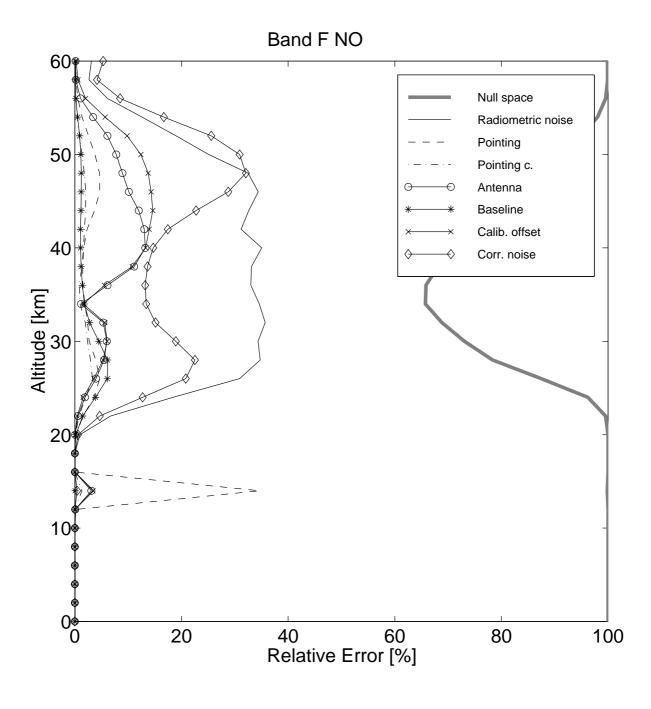


## Summary: Temperature Band F (near 954 GHz)



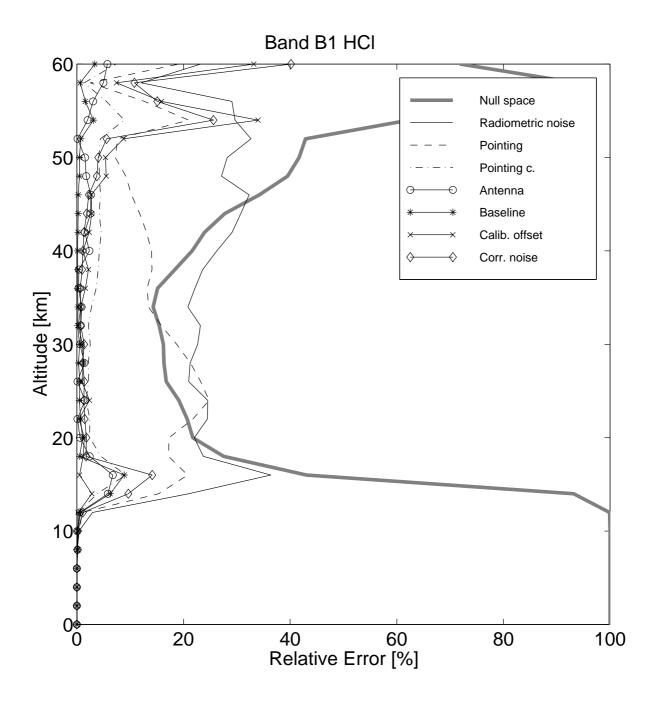


## Summary: NO Band F (near 954 GHz)



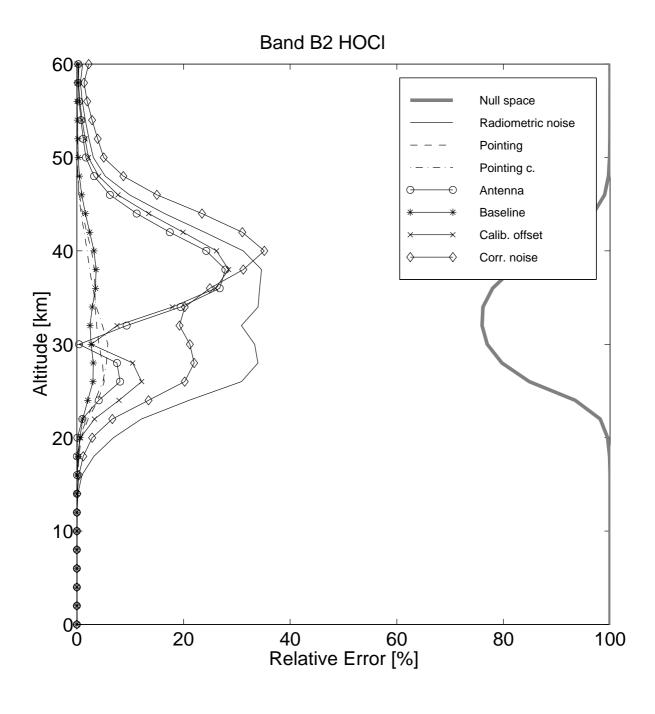


# Summary: HCI Band B1 (near 626 GHz)



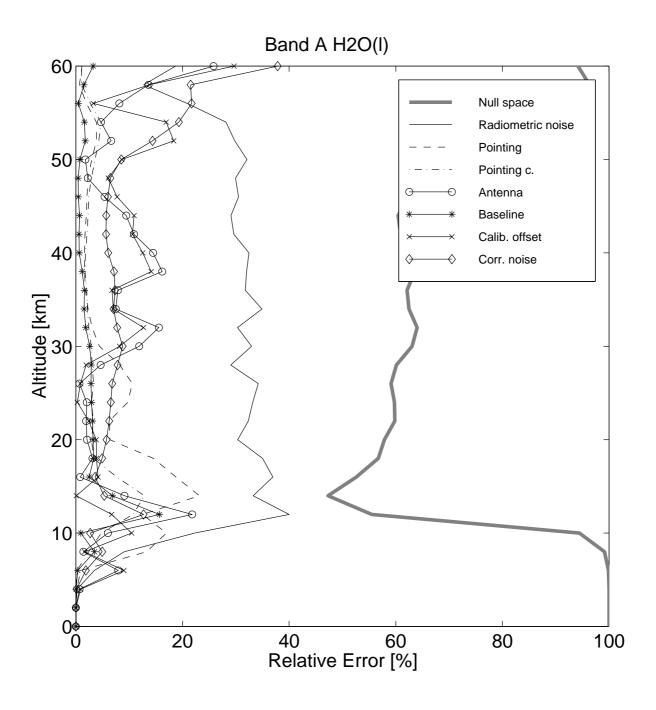


## Summary: HOCI Band B2 (near 628 GHz)



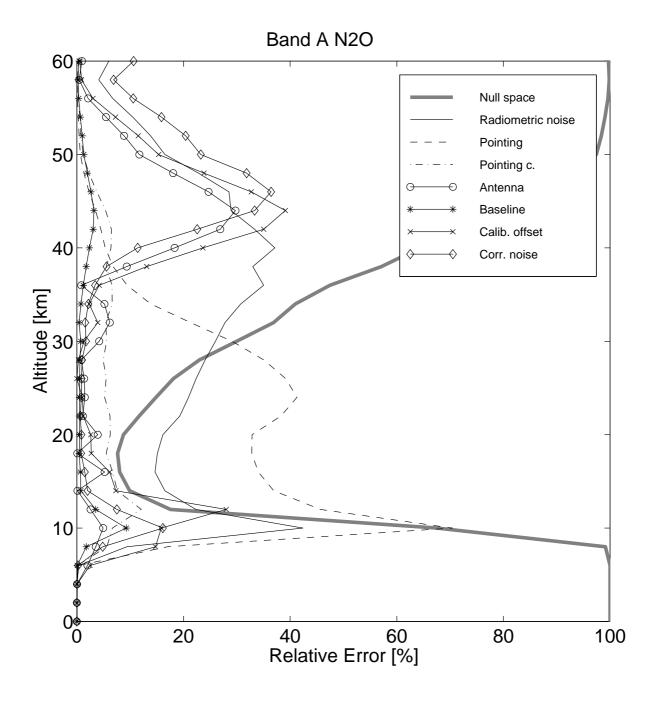


# Summary: H<sub>2</sub>O Band A (near 500 GHz)





# Summary: N<sub>2</sub>O Band A (near 500 GHz)





### **Conclusions (1)**

#### Most critical parameters:

- Antenna pattern knowledge (far wing must be covered, requires ≤ 35 dB noise)
- Pointing accuracy (should be better than ± 200 m RMS, increased delay in antenna control loop helps)
- Unwanted sideband (should be significantly better than 20 dB if there are strong lines in the sideband)
  - Can be optimized if other sideband is not used for measurements
- Atmospheric Temperature uncertainty
  - Temperature retrieval schemes are currently investigated



### **Conclusions (2)**

#### Slightly less critical parameters:

- Baseline ripples
- Calibration errors

### But SOPRANO radiometric requirements are stringent (one could also say optimistic):

- 0.1 K amplitude of baseline ripples
- 1 K hot and cold load temperature errors
- 0.2 K non-linearity

More significant for SMILES because radiometric noise is lower

From all our practical experience, baseline ripples are likely to be a problem with the actual instrument.



### Conclusions (3)

### Relatively uncritical parameters:

- Actual shape of antenna pattern (investigated 1–10% near wing, 0–4% far wing)
  - provided it is well known
  - provided FWHM stays the same
  - provided the scan goes down into the opaque region
- Pointing stability
  - Leads to slightly increased width of effective antenna pattern
  - $-\pm 200\,\mathrm{m}$  is tolerable
- Baseline discontinuities (0.4 K every 2 GHz is tolerable)
  - Can be optimized (disc. not on line centers)
- Correlated noise
  - Same order of magnitude as measurement noise (for integration time 10 × atmospheric)
  - Statistical error, i.e., goes down when data is averaged



#### Conclusion of the conclusions

#### Crucial!

- Pointing accuracy
- Baseline
- Knowledge of instrument parameters, in particular
  - Antenna pattern
  - Sideband ratio



### **Ongoing work**

The study has been extended by ESTEC. Issues:

- Temperature / pointing retrieval (in particular from bands without oxygen lines):
  IFE Bremen
- Dedicated study for the retrieval of very weak species, e.g., BrO:

Observatoire de Bordeaux

